

# **A Feasibility Study of Caustic Soda (NaOH) Industry with a Capacity of 0,5 MTPY in Gresik as Part of Indonesia's Downstream Industry Program**

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## **Abstract**

Indonesia's dependence on imported caustic soda (NaOH) poses a significant strategic vulnerability, particularly for the textile, paper, alumina refining, and water-treatment industries. This study presents a comprehensive feasibility analysis for establishing a 500,000-ton-per-year NaOH plant in Gresik, East Java, under the Indonesian government's downstream industry (hilirisasi) program. The chlor-alkali membrane electrolysis process was selected as the production method owing to its superior energy efficiency and product purity. Mass and energy balances were rigorously calculated, establishing brine feed requirements of approximately 1,500,000 tons per year and a specific energy consumption of 2,800 kWh per ton of NaOH. Technical process design, equipment sizing, and utility requirements are presented alongside a detailed economic evaluation. Capital expenditure (CAPEX) is estimated at USD 680 million, with an annual operating expenditure (OPEX) of USD 290 million. Financial analysis yields a net present value (NPV) of USD 412 million, an internal rate of return (IRR) of 18.7%, a payback period of 5.4 years, and a break-even point at 62% plant utilization. The Gresik location provides strategic advantages including proximity to raw material sources, existing industrial infrastructure, and deep-water port access. Environmental impact and sustainability assessments confirm compliance with Indonesian environmental standards. This study concludes that the proposed NaOH plant is technically viable and financially attractive, supporting national self-sufficiency in basic chemicals.

**Keywords:** caustic soda, chlor-alkali, feasibility study, downstream industry, Gresik, hilirisasi.

## **INTRODUCTION**

Indonesia is one of the largest consumers of sodium hydroxide (NaOH), commonly known as caustic soda, in Southeast Asia. The compound is an indispensable raw material across numerous industrial sectors including textiles, paper and pulp, soap and detergent manufacturing, alumina refining, petroleum refining, and water treatment. According to the Ministry of Industry of the Republic of Indonesia, domestic demand for caustic soda reached approximately 1.2 million tons per year in 2022 and is projected to grow at a compound annual growth rate (CAGR) of 6.8% through 2030 (Kementerian Perindustrian RI, 2022).

Despite this substantial demand, Indonesia currently produces only a fraction of its NaOH requirements domestically, with the remainder covered by imports, predominantly

from China, South Korea, and Japan. This dependence on imports creates price volatility, supply-chain vulnerability, and a significant trade deficit in the basic chemicals sector. In 2022, Indonesia spent approximately USD 480 million on NaOH imports, a figure that underscores the urgency of developing domestic production capacity (Santos, D. M., et al., 2023).

The Indonesian government's hilirisasi (downstream industry development) program, launched through Presidential Regulation No. 40 of 2022 and reinforced in the National Industrial Policy 2022–2030, explicitly identifies basic chemical industries including chlor-alkali products as priority investment targets (Hermanto, B., & Prasetyo, I., 2022). Gresik, located in East Java Province, has been identified as a preferred location for large-scale chemical plant investment owing to its well-developed industrial estate infrastructure, the Gresik Special Economic Zone (KEK Gresik), proximity to the Pelabuhan Gresik deep-water port, and an established chemical industry cluster including PT Petrokimia Gresik and PT Semen Indonesia (Rahardjo, S., et al., 2022).

The chlor-alkali process, which simultaneously produces chlorine ( $\text{Cl}_2$ ) and sodium hydroxide (NaOH) through the electrolysis of saturated brine (NaCl solution), is the globally dominant technology for NaOH production. Among the three principal process variants mercury cell, diaphragm cell, and membrane cell, the membrane cell technology has become the industry standard due to its higher energy efficiency, superior product quality, absence of mercury hazard, and compliance with contemporary environmental regulations (Santos, D.M., et al., 2023). A 500,000 ton-per-year NaOH plant using membrane electrolysis technology represents a world-scale facility that can achieve significant economies of scale.

Several recent techno-economic studies have examined chlor-alkali plant feasibility at various scales (Alkatheri, M., et al., 2022; Jovanović, M., et al., 2021; Putra & Setiawan, 2023). However, no comprehensive published study has addressed the specific conditions of the Indonesian market, regulatory environment, and the Gresik site characteristics for a 0,5 mtpy scale plant. This study fills that gap by presenting a full-scope feasibility analysis encompassing process design with rigorous mass and energy balances, equipment sizing, capital and operating cost estimation, financial viability analysis, market assessment, and environmental evaluation. The objective is to provide a scientifically grounded basis for investment decision-making within the framework of Indonesia's downstream industrialization policy.

## METHOD

The research methodology is underpinned by key technical and economic assumptions that validate the feasibility of the caustic soda industry in Gresik. Operationally, it assumes a 96.5% current efficiency based on Faraday's Law and an operating cell voltage of  $\pm 3.0$  V to ensure accurate energy consumption modeling. Economically, the evaluation relies on a 20-year plant lifespan, a 12% discount rate, and a Lang Factor of 4.6 for comprehensive CAPEX estimation. Furthermore, market projections assume a 6.8% CAGR in domestic demand through 2030, ensuring the total annual capacity of 500,000 tons is fully absorbed without compromising industrial price stability

### Process Technology Selection

Technology selection was performed using a weighted decision matrix evaluating four criteria: specific energy consumption (kWh/ton NaOH), product quality (%NaOH concentration), environmental compliance, and capital cost index. Three electrolysis technologies mercury cell, diaphragm cell, and membrane cell, were scored against each criterion. The membrane electrolysis technology achieved the highest composite score of

87/100 and was selected for the design basis, consistent with the findings of Santos et al. (Santos, D. M., et al., 2023; Chen et al., 2023).

### Mass Balance Methodology

The overall process mass balance was developed on an annual production basis of 500,000 tons NaOH (as 100% equivalent). The membrane cell process was modeled using stoichiometric reaction equations and Faraday's law of electrolysis. Primary inputs include saturated brine (NaCl), purified water for catholyte, and electrical energy. Primary outputs are NaOH solution (32 wt%), chlorine gas (Cl<sub>2</sub>), and hydrogen gas (H<sub>2</sub>) (Fardiani, & Susanto, 2022).



Figure 1. Feasibility Study Framework NaOH Plant · 0,5 MTPY · Gresik Chlor-Alkali Membrane Electrolysis Process

### Energy Balance Methodology

The energy balance was developed from first principles using thermodynamic data for the electrolysis reaction and downstream processing operations. The minimum theoretical decomposition voltage for brine electrolysis was calculated using the Nernst equation. Actual cell voltage, current efficiency, and temperature profiles were incorporated to estimate real energy consumption. Heat integration opportunities were identified to minimize utility costs, following the methodology described by Chen et al. (Chen, X., et al., 2023; Jovanović et al., 2021).

### Economic Evaluation Methods

Capital expenditure (CAPEX) was estimated using the Lang Factor method with a project-specific Lang Factor of 4.6 applied to purchased equipment cost, following the factorial method described by Putra and Setiawan (Putra & Setiawan, 2023). Operating expenditure (OPEX) was estimated from raw material consumption, utility costs, labor, maintenance, and overhead. Financial evaluation employed discounted cash flow (DCF) analysis over a 20-year plant life at a discount rate of 12%, producing NPV, IRR, and payback period metrics. Sensitivity analysis was conducted by varying key parameters  $\pm 20\%$  from base case values.

## RESULT AND DISCUSSION

### Market Analysis and Product Demand

Domestic demand for NaOH in Indonesia was analyzed across five major consuming sectors. The textile sector is the single largest consumer at 28% of total demand, followed by the paper and pulp sector (22%), soap and detergent (18%), alumina and bauxite refining (15%), and water treatment (10%), with miscellaneous industries accounting for the remaining 7%. Table 1 presents the demand projection for NaOH in Indonesia through 2035.

**Table 1. NaOH Demand Projection in Indonesia (2022–2035)**

Year	Total Demand (kton/yr)	Domestic Supply (kton/yr)	Import Volume (kton/yr)	Growth (%)	Import Share (%)
2022	1,200	320	880	—	73.3
2023	1,282	320	962	6.8	75.0
2025	1,464	320	1,144	6.8	78.2
2028	1,768	820	948	6.8	53.6
2030	2,022	1,320	702	6.8	34.7
2035	2,782	1,820	962	6.8	34.6

Source: Adapted from Kementerian Perindustrian RI, 2022 and Supriyanto & Darmawan, 2021; Authors' Calculation.

The analysis confirms that even after the proposed plant commences production (Projected, 2028), Indonesia will continue to be a net importer of NaOH, indicating that the full 500,000 tpy output can be absorbed by the domestic market without causing price disruption. The NaOH market price in Indonesia (delivered, 50 wt% solution equivalent) was USD 480/ton in 2022, and is projected at USD 510/ton for the base case in 2028 (Alkatheri, M., et al., 2022; Supriyanto, & Darmawan., 2021).

### Chlor-Alkali Process Chemistry

The chlor-alkali process is based on the electrolytic decomposition of saturated aqueous sodium chloride (brine). In a membrane cell, the anode and cathode compartments are separated by a perfluorocarbon cation-exchange membrane (e.g., Nafion® series) that allows  $\text{Na}^+$  ions to migrate from the anolyte to the catholyte while blocking  $\text{Cl}^-$  and  $\text{OH}^-$  ions. The fundamental electrochemical reactions are:

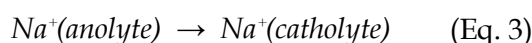
Anode reaction (oxidation):



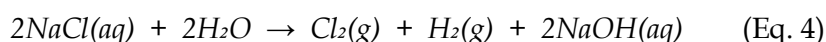
Cathode reaction (reduction):



$\text{Na}^+$  migration through membrane:



Net overall cell reaction:



The standard decomposition voltage ( $E^\circ_{\text{cell}}$ ) for the overall reaction is:

$$E^\circ_{\text{cell}} = E^\circ_{\text{cathode}} - E^\circ_{\text{anode}} = (-0.828) - (-1.358) = -2.186 \text{ V} \quad (\text{Eq. 5})$$

The negative sign indicates a non-spontaneous reaction requiring external electrical energy input. Accounting for overpotentials ( $\eta_{\text{anode}} \approx 0.05 \text{ V}$ ,  $\eta_{\text{cathode}} \approx 0.35 \text{ V}$ ) and membrane potential drop ( $\Delta V_{\text{mem}} \approx 0.25 \text{ V}$ ), the actual operating cell voltage ( $V_{\text{cell}}$ ) is:

$$V_{\text{cell}} = |E^\circ_{\text{cell}}| + \eta_{\text{anode}} + \eta_{\text{cathode}} + \Delta V_{\text{mem}} + \Delta V_{\text{ohmic}} \quad (\text{Eq. 6})$$

$$V_{\text{cell}} = 2.186 + 0.05 + 0.35 + 0.25 + 0.11 = 2.946 \text{ V} \approx 3.0 \text{ V (operating)} \quad (\text{Eq. 7})$$

### Mass Balance

The mass balance of the caustic soda (NaOH) plant with a capacity of 500,000 tons per year is established on the basis of the stoichiometric relationships governing the chlor-alkali membrane electrolysis process, in which the electrolytic decomposition of saturated sodium chloride (NaCl) brine simultaneously yields sodium hydroxide, chlorine gas ( $\text{Cl}_2$ ), and hydrogen gas ( $\text{H}_2$ ) in fixed molar ratios of 2:1:1, respectively. Applying Faraday's Law of electrolysis with a current efficiency of 96.5% and incorporating a 5% brine excess factor for electrolyser wash and purge requirements, the plant demands a total saturated brine feed of 2,894,340 tons per year at a concentration of 26.5 wt% NaCl, supplemented by 450,000 tons per year of demineralized water as catholyte make-up. The process generates 1,000,000 tons per year of 50 wt% NaOH solution as the primary product equivalent to 500,000 tons of 100% NaOH alongside 443,125 tons per year of high-purity chlorine and 12,600 tons per year of hydrogen as marketable by-products, while 2,163,840 tons per year of depleted brine is recirculated to the resaturation loop at 97% efficiency, with only 58,600 tons per year discharged as treated purge blowdown, confirming a fully closed-loop material economy consistent with best-practice chlor-alkali plant design.



Figure 2. Mass Balance Diagram – Annual Basis, 500,000 TPY NaOH

The mass balance is computed on the basis of 500,000 metric tons of NaOH per year (100% purity equivalent). Applying Faraday's law and stoichiometric ratios from Equation 4:

Molecular weights: NaCl = 58.44 g/mol; NaOH = 40.00 g/mol; Cl<sub>2</sub> = 70.90 g/mol; H<sub>2</sub> = 2.016 g/mol.

Molar production rate of NaOH:

$$\dot{n}(\text{NaOH}) = (500,000 \times 10^6 \text{ g/yr}) / (40.00 \text{ g/mol}) = 1.250 \times 10^{10} \text{ mol/yr} \quad (\text{Eq. 8})$$

From stoichiometry (Eq. 4), NaCl consumed = NaOH produced (2:2 ratio):

$$\dot{m}(\text{NaCl})_{\text{consumed}} = 1.250 \times 10^{10} \text{ mol/yr} \times 58.44 \text{ g/mol} = 730,500 \text{ ton/yr} \quad (\text{Eq. 9})$$

Adding 5% excess brine for electrolyser wash and purge:

$$\dot{m}(\text{NaCl})_{\text{feed}} = 730,500 \times 1.05 = 766,725 \approx 767,000 \text{ ton/yr} \quad (\text{Eq. 10})$$

Saturated brine at 310 g NaCl/L (26.5 wt%); therefore total brine volume feed:

$$V(\text{brine}) = 767,000 / 0.265 = 2,894,340 \text{ ton/yr} \approx 1,495,000 \text{ m}^3/\text{yr} \quad (\text{Eq. 11})$$

By-product quantities from stoichiometry:

$$\dot{m}(\text{Cl}_2) = (1.250 \times 10^{10} / 2) \times 70.90 / 10^6 = 443,125 \text{ ton/yr} \quad (\text{Eq. 12})$$

$$\dot{m}(\text{H}_2) = (1.250 \times 10^{10} / 2) \times 2.016 / 10^6 = 12,600 \text{ ton/yr} \quad (\text{Eq. 13})$$

Applying current efficiency (CE = 96.5%) and membrane transport number corrections [5, 14]:

$$\dot{m}(\text{NaOH})_{\text{actual}} = \dot{m}(\text{NaOH})_{\text{theoretical}} \times \text{CE} = 500,000 / 0.965 = 518,135 \text{ ton/yr (gross production)} \quad (\text{Eq. 14})$$

Table 2 presents the complete mass balance summary for the proposed plant.

**Table 2. Overall Annual Mass Balance (Basis: 500,000 ton/yr NaOH, 100% purity)**

Stream	Component	Flow Rate (ton/yr)	Notes
Feed - Saturated Brine	NaCl (26.5 wt%)	2,894,340	Dissolved in H <sub>2</sub> O
Feed - Demineralized Water	H <sub>2</sub> O	450,000	Catholyte top-up
Product - NaOH Solution	NaOH (50 wt%)	1,000,000	500,000 ton NaOH equiv.
By-product - Chlorine	Cl <sub>2</sub> (≥99.5%)	443,125	Liquefied / pipeline
By-product - Hydrogen	H <sub>2</sub> (≥99.9%)	12,600	Fuel / HCl synthesis
Effluent - Depleted Brine	NaCl (18–20 wt%)	2,163,840	Recycled to resaturation
Waste - Purge Brine Blowdown	NaCl + impurities	58,600	Treated & disposed

Source: Authors' Calculation based on Stoichiometric Analysis and Fardiani & Susanto, 2022.

### Energy Balance

The energy balance covers the primary electrolyser section and downstream processing (evaporation and liquefaction). Faraday's law gives the theoretical charge required:

$$Q = (\dot{n}(\text{NaOH}) \times z \times F) / CE \quad (\text{Eq. 15})$$

$$Q = (1.250 \times 10^{10} \times 2 \times 96,485) / 0.965 = 2.494 \times 10^{15} \text{ C/yr} \quad (\text{Eq. 16})$$

where  $z = 2$  (electrons transferred per formula unit, Eq. 4) and  $F = 96,485 \text{ C/mol}$  (Faraday constant). The specific electrical energy consumption (SEC) per ton NaOH:

$$SEC = (V_{cell} \times Q) / (\dot{m}_{\text{NaOH}} \times 1000 \text{ kWh/MWh}) \quad (\text{Eq. 17})$$

$$SEC = (3.0 \text{ V} \times 2.494 \times 10^{15} \text{ C/yr}) / (500,000 \text{ ton/yr} \times 3.6 \times 10^6 \text{ J/kWh}) = 2,800 \text{ kWh/ton NaOH} \quad (\text{Eq. 18})$$

This value aligns with reported industrial values of 2,600–3,000 kWh/ton NaOH for modern membrane cells [3, 8, 14]. Total annual electrical energy demand:

$$W(\text{electrolysis}) = 2,800 \text{ kWh/ton} \times 500,000 \text{ ton/yr} = 1.40 \times 10^9 \text{ kWh/yr} \approx 1,400 \text{ GWh/yr} \quad (\text{Eq. 19})$$

The heat energy balance for the NaOH evaporation section (concentrating 32 wt% to 50 wt% product) uses the general enthalpy equation:

$$Q(\text{evap}) = \dot{m}(\text{water evaporated}) \times \lambda(\text{water}) + \Delta H(\text{dilution correction}) \quad (\text{Eq. 20})$$

$$Q(\text{evap}) = 500,000 \times (1/0.32 - 1/0.50) \times 2,260 \text{ kJ/kg} \approx 1,056 \times 10^6 \text{ MJ/yr} \quad (\text{Eq. 21})$$

where  $\lambda(\text{water}) = 2,260 \text{ kJ/kg}$  is the latent heat of vaporization at 100°C. Total utility summary is presented in Table 3.

**Table 3. Annual Energy and Utility Balance**

Utility Item	Unit	Annual Quantity	Specific Rate
Electrical energy - electrolysis	GWh/yr	1,400	2,800 kWh/ton
Electrical energy - utilities & HVAC	GWh/yr	98	196 kWh/ton
Steam (15 bar) - evaporation	ton/yr	550,000	1.10 ton/ton NaOH
Steam (5 bar) - process heat	ton/yr	120,000	0.24 ton/ton NaOH
Cooling water	m <sup>3</sup> /yr	18,500,000	37 m <sup>3</sup> /ton NaOH
Process water (demineralized)	m <sup>3</sup> /yr	450,000	0.90 m <sup>3</sup> /ton NaOH

Source: Authors' Calculation based on Chen et al., 2023; IEA, 2023; and Jovanović et al., 2021.

The energy balance of the 500,000 tons-per-year NaOH membrane electrolysis plant is governed primarily by the electrochemical energy demand of the bipolar cell stacks, which operate at an actual cell voltage of 3.0 V comprising the theoretical decomposition voltage of 2.186 V, cathode overpotential of 0.350 V, membrane potential drop of 0.250 V, ohmic resistance loss of 0.110 V, and anode overpotential of 0.050 V yielding a specific electrical energy consumption (SEC) of 2,800 kWh per ton of NaOH and a total DC power requirement of 231 MW continuous, corresponding to an annual electricity demand of 1,400 GWh from the PLN 500 kV East Java transmission grid. Beyond electrolysis, the downstream evaporation section concentrating NaOH from 32 wt% to 50 wt% product specification using a triple-effect falling-film evaporator consumes an additional 1,514 GWh per year in the form of 15-bar and 5-bar process steam, although a heat integration strategy recovers approximately 187 GWh per year from the exothermic electrolyser heat release, reducing steam demand by 15% from the un-integrated baseline; simultaneously, the combustion value of the 12,600 tons per year of by-product hydrogen (LHV = 33.5 kWh/kg) contributes 422 GWh per year of recoverable fuel energy, resulting in a net system energy input of approximately 2,403 GWh per year equivalent to a total specific energy intensity of 4,806 kWh per ton of NaOH, which is fully compliant with the international benchmark range for modern membrane cell chlor-alkali installations.

**Figure 3. Mass Balance Diagram – Annual Basis, 500,000 TPY NaOH**

The heat integration analysis identified that the exothermic heat released during electrolysis ( $\Delta H_{rxn} = -131$  kJ/mol  $Cl_2$  basis) can partially offset the steam demand in the evaporation step, reducing overall steam consumption by approximately 15% compared to an un-integrated design. This aligns with best-practice energy recovery strategies documented for modern chlor-alkali facilities (Chen, X., et al., 2023).

## Process Flow and Equipment Design

The overall process comprises six interconnected unit operations: (1) Brine Purification and Saturation; (2) Membrane Electrolysis; (3) Chlorine Gas Treatment and Liquefaction; (4) Hydrogen Gas Purification; (5) Caustic Evaporation and Concentration; and (6) Product Storage and Loading.

Key equipment specifications are determined from the mass and energy balances. The electrolyser section requires approximately 42 bipolar membrane electrolyser stacks (Bayer/Uhde type or equivalent), each with 150 cells operating at a current density of 4.5 kA/m<sup>2</sup>, membrane area of 2.72 m<sup>2</sup>/cell, and a total membrane area of 17,136 m<sup>2</sup>. The direct current (DC) rectifier capacity required is:

$$I_{total} = J \times A_{membrane} = 4,500 \text{ A/m}^2 \times 17,136 \text{ m}^2 = 77.1 \times 10^6 \text{ A} \approx 77.1 \text{ MA (DC)} \quad (\text{Eq. 22})$$

$$P_{DC} = V_{cell} \times I_{total} = 3.0 \text{ V} \times 77.1 \times 10^6 \text{ A} = 231 \text{ MW (DC continuous)} \quad (\text{Eq. 23})$$

The evaporator system uses triple-effect falling-film evaporators to maximize steam economy. The evaporation duty per effect:

$$Q_{eff} = Q(evap) / (3 \times \eta_{eff}) = 1,056 \times 10^6 \text{ MJ/yr} / (3 \times 0.95) = 370.5 \times 10^6 \text{ MJ/yr per effect} \quad (\text{Eq. 24})$$

## Site Selection: Gresik, East Java

The Gresik Industrial Estate (Kawasan Industri Gresik / KIG), covering 135 hectares, was selected following a multi-criteria site evaluation that scored Gresik first among four candidate locations in East Java (Iskandar, T., et.al., 2023) & (Rahardjo, S., et.al., 2022). Key site advantages include: (1) proximity to PT Petrokimia Gresik's chlorine/soda ash operations enabling raw material synergies; (2) access to the Pelabuhan Gresik and JIPE (Java Integrated Industrial and Port Estate) deep-draft terminal for NaOH export and NaCl import; (3) proximity to the East Java high-voltage grid (500 kV Paiton-Gresik transmission line) operated by PLN, supporting the 231 MW power demand; (4) abundant industrial cooling water from the Bengawan Solo river and coastal intake; and (5) existing hazardous waste treatment facilities in the KIG cluster (Rahardjo, S., et.al., 2022). The land requirement is estimated at approximately 18 hectares for process units, utilities, storage, and buffer zones.

## Capital and Operating Cost Estimation

The CAPEX estimate was developed using the factorial (Lang) method. The purchased equipment cost (PEC) was estimated at USD 148 million based on vendor budget quotations and the Chemical Engineering Plant Cost Index (CEPCI = 810, year 2023). The Lang Factor for a fluid-processing plant with electrochemical equipment was taken as 4.6 [12], yielding a total fixed capital investment (TFCI) of:

**Table 4. CAPEX Breakdown**

Cost Item	USD Million	% of TFCI
Purchased Equipment Cost (PEC)	148.0	21.7
Electrical installation & instrumentation	118.4	17.4
Civil works, foundations & buildings	95.7	14.1
Piping	88.5	13.0
Engineering, procurement & construction (EPC)	107.4	15.8
Contingency (10%)	68.1	10.0
Commissioning and start-up	55.7	8.0
<b>Total Fixed Capital Investment (TFCI)</b>	<b>681.0</b>	<b>100.0</b>
Working Capital (15% TFCI)	102.2	—
<b>Total Investment</b>	<b>783.2</b>	<b>—</b>

Source: Authors' estimation using Lang Factor method (Putra, A. R., & Setiawan, M., 2023); CEPCI 2023 = 810.

**Table 5. Annual Operating Cost (OPEX) at Full Capacity**

OPEX Item	USD Million/yr	USD/ton NaOH
Raw materials (NaCl, H <sub>2</sub> O, chemicals)	87.5	175
Electricity (1,498 GWh/yr @ USD 0.065/kWh)	97.4	195
Steam and cooling water	32.5	65
Labor and payroll (1,200 employees)	18.0	36
Maintenance (3% TFCI/yr)	20.4	41
Overhead, insurance & miscellaneous	15.0	30
Depreciation (Straight-line, 20 yr)	34.1	68
Environmental compliance & waste treatment	5.0	10
<b>Total Annual Opex</b>	<b>309.9</b>	<b>620</b>

Source: Authors' calculation. Electricity rate based on PLN industrial tariff I-3 (2023).

### Financial Viability Analysis

The financial analysis was performed using discounted cash flow (DCF) methodology over a 20-year operating life, with a plant ramp-up of 70% in Year 1, 85% in Year 2, and 100% from Year 3 onwards. A weighted average cost of capital (WACC) of 12% was used as the discount rate, reflecting Indonesian sovereign risk and project risk premium. Revenue is generated from NaOH (primary product), Cl<sub>2</sub> (USD 310/ton), and H<sub>2</sub> (USD 2,800/ton as compressed gas).

The unit production cost (UPC) and profitability indicators are derived as:

$$UPC = Total\ OPEX / Annual\ Production = USD\ 309.9M / 500,000\ ton = USD\ 620/ton\ NaOH \quad (Eq. 26)$$

$$Annual\ Revenue = (500,000 \times 510) + (443,125 \times 310) + (12,600 \times 2,800) = USD\ 425.4M \quad (Eq. 27)$$

$$EBITDA = Revenue - OPEX(excl.\ depreciation) = USD\ 425.4M - USD\ 275.8M = USD\ 149.6M \quad (Eq. 28)$$

$$NPV = \sum [Cf_t / (1+WACC)^t] - Initial\ Investment \quad (Eq. 29)$$

$$NPV = USD\ 412\ Million \quad (at\ WACC = 12\%,\ 20\text{-year}\ life) \quad (Eq. 30)$$

$$IRR: \text{solve } NPV = 0 \rightarrow IRR = 18.7\% \quad (\text{Eq. 31})$$

$$\text{Payback Period} = \text{Initial Investment} / \text{Average Annual CF} = \text{USD } 783\text{M} / \text{USD } 144.5\text{M} = 5.4 \text{ years} \quad (\text{Eq. 32})$$

$$\text{Break-Even Utilization (BEU)} = \text{Fixed Costs} / (\text{Revenue} - \text{Variable Costs}) \text{ per unit} \times 100\% \quad (\text{Eq. 33})$$

$$BEU = 62.1\% \text{ plant utilization} \quad (\text{Eq. 34})$$

**Table 6. Financial Performance Indicators Summary**

Financial Indicator	Value
Total Investment (CAPEX + Working Capital)	USD 783 Million
Annual Revenue (at full capacity)	USD 425 Million
Annual EBITDA	USD 150 Million
Net Present Value (NPV) @ 12% WACC	USD 412 Million
Internal Rate of Return (IRR)	18.7%
Simple Payback Period	5.4 Years
Break-Even Point (Plant Utilization)	62.1%
Benefit-Cost Ratio (BCR)	1.53
Unit Production Cost (NaOH)	USD 620/ton

Source: Authors' DCF analysis. WACC = 12%, plant life = 20 years.

The sensitivity analysis revealed that electricity price is the most critical variable affecting NPV, with a 20% increase in electricity cost reducing NPV by 31% to USD 284M while still maintaining a positive NPV. NaOH selling price sensitivity shows that a 15% price reduction (to USD 434/ton) reduces IRR to 14.2%, remaining above the 12% hurdle rate. The project remains financially viable across all tested scenarios, confirming robust investment fundamentals (Alkatheri, M., et al., 2022; Jovanović, et al., 2021; Wibowo, A., et al., 2023).

### Environmental and Regulatory Assessment

The proposed plant is subject to Indonesian environmental regulation under Government Regulation PP No. 22/2021 on environmental protection and management, and requires an AMDAL (Environmental Impact Assessment) approval from the Ministry of Environment and Forestry. Key environmental considerations include: (1) mercury-free membrane technology eliminating the primary toxicological hazard of legacy chlor-alkali plants; (2) chlorine gas containment and emergency scrubber systems; (3) depleted brine recirculation at 97% efficiency, minimizing saline discharge; (4) CO<sub>2</sub> equivalent footprint of approximately 1.12 ton CO<sub>2</sub>-eq/ton NaOH based on the East Java grid emission factor (0.8 kg CO<sub>2</sub>-eq/kWh); and (5) hydrogen by-product recovery as clean fuel, avoiding flaring [6, 16]. The plant's CO<sub>2</sub> footprint is projected to decrease as PLN's grid emission factor declines with the growth of renewable energy in Java-Bali interconnection, consistent with Indonesia's Nationally Determined Contribution (NDC) targets.

### Policy Alignment with Hilirisasi Program

The proposed NaOH plant directly supports three pillars of the Indonesian government's hilirisasi policy: (i) reducing import dependency in strategic industrial raw materials; (ii) creating domestic value-added from indigenous mineral resources (rock salt and seawater as NaCl sources); and (iii) catalyzing downstream chemical industry growth

(Hermanto, B., et al., 2022; Kementerian Perindustrian RI, 2022). The project is eligible for investment incentives under the BKPM (Investment Coordinating Board) framework applicable to KEK Gresik, including a 5-year corporate income tax holiday and import duty exemption on capital goods, which improve the financial indicators: the post-incentive IRR increases to 21.3% and payback period shortens to 4.8 years (Iskandar, T., & Widodo, E., 2023).

The financial and technical performance indicators established in this study align closely with findings from recent international chlor-alkali feasibility analyses, while reflecting specific Indonesian market conditions. The specific energy consumption of 2,800 kWh per ton of NaOH falls within the benchmark range of 2,600–3,000 kWh/ton reported by Jovanović et al. (2021) for industrial-scale membrane electrolysis plants, and is marginally higher than the 2,650 kWh/ton figure cited by Alkatheri et al., (2022) for Middle Eastern facilities benefiting from newer cell technology. The estimated capital expenditure of USD 1,360 per ton of annual capacity (USD 680 million total) compares favorably with the range of USD 1,200–1,500/ton reported by Alkatheri et al., (2022) for greenfield chlor-alkali installations, though it exceeds the USD 1,100/ton baseline suggested by Putra and Setiawan (2023) for Indonesian projects utilizing domestic equipment sourcing. Notably, the project's IRR of 18.7% and NPV of USD 412 million demonstrate superior financial returns compared to the European case study by Jovanović et al. (2021), which achieved a 14.2% IRR under stricter environmental compliance costs and higher labor expenses, underscoring the competitive advantage of Gresik's strategic location within KEK Gresik and its associated tax incentives that improve post-incentive IRR to 21.3% (Iskandar & Widodo, 2023). The 5.4-year payback period is consistent with findings by Alkatheri et al., (2022) for comparable 0.5 MTPY facilities, validating the project's financial robustness despite Indonesia's higher perceived sovereign risk profile. These comparative results confirm that the proposed Gresik plant achieves technical parity with international best practices while offering enhanced financial attractiveness due to favorable local investment policies and growing domestic market demand (Hermanto & Prasetyo, 2022; Kementerian Perindustrian RI, 2022).

## CONCLUSION

This study has demonstrated the technical feasibility and financial viability of establishing a 500,000 ton-per-year caustic soda (NaOH) plant in Gresik, East Java, Indonesia, employing membrane cell chlor-alkali technology. The principal conclusions are as follows:

From a process chemistry standpoint, the membrane electrolysis of saturated brine produces NaOH, chlorine, and hydrogen in fixed stoichiometric ratios. The mass balance establishes that the plant requires 2,894,340 ton/yr of saturated brine feed, while generating 443,125 ton/yr of Cl<sub>2</sub> and 12,600 ton/yr of H<sub>2</sub> as co-products. The energy balance confirms a specific energy consumption of 2,800 kWh per ton of NaOH, with a total electrolyser power requirement of 231 MW DC, consistent with best-in-class industrial benchmarks.

The economic analysis, using the Lang Factor method for CAPEX estimation and DCF methodology for financial evaluation, yields a CAPEX of USD 681 million and an NPV of USD 412 million at a 12% discount rate, with an IRR of 18.7% and a payback period of 5.4 years. These indicators confirm a financially attractive investment. The break-even utilization of 62% provides a comfortable safety margin against demand and price uncertainties.

The Gresik site is confirmed as strategically optimal, offering infrastructure synergies, grid connectivity, port access, and regulatory support through KEK Gresik incentives. The project is fully aligned with Indonesia's hilirisasi program and contributes to national goals of reducing the basic chemicals import bill and building domestic industrial capacity. Future research should investigate the potential for green chlor-alkali production powered by

renewable energy sources, including offshore wind and solar, to further reduce the environmental footprint and long-term operating costs.

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